

Reverse Engineering

For a given plane (e.g. B747-400), the following parameters are known: λ_{LFL} , λ_{TOFL} , V_{app} , $R @ \text{max payload}$, b , m_{nro} / S , m_L / m_{nro} , m_{oe} , m_{nro} , m_{oe} / m_{nro} , T_{ro} , $T_{ro} / (m_{nro} \cdot g)$, V_{cr} , h_{cr} , Π , $\eta_{PAX, std}$, $\eta_{PAX, max}$, m_{PL} , BPR.

The following values can be easily calculated:

$$S = 541,2 \text{ m}^2$$

$$A = \frac{b^2}{S}$$

Other values are unknown, the companies secrets:

- SFC
- $E = \frac{L}{D}$
- $C_{L, max, L}$

These parameters can be found by reverse engineering.

PLAN:

- reverse the excel-file
 - make a list of the known parameters; add the calculated values - calculate the percentage of deviation for each parameter
 - make the squared sum of the deviation
 - make a list that contains the parameters we can change - this includes an upper and lower limit (according to skybrary)
- => Make a solver that minimizes the squared sum by changing the parameters in between the limits from skybrary.

Normale gang van zaken:

* E_{\max} wordt berekend volgens Lofth of Raymer

$$E_{\max} = k_E \cdot \sqrt{\frac{A}{S_{\text{ref}}/S_{\text{ref}}}} \quad \text{met} \quad k_E = \frac{1}{2} \cdot \sqrt{\frac{\bar{u} \cdot c}{g}} = 14,9 \quad (\text{Lofth})$$

$$k_E = 15,8 \quad (\text{Raymer})$$

$$* E = \frac{2 \cdot E_{\max}}{\frac{C_{l,m}}{C_l} + \frac{C_l}{C_{l,m}}}$$

$$* \frac{T_{\text{ro}}}{m_{\text{ro}} \cdot f} = \frac{1}{\frac{T_{\text{ce}}}{T_{\text{ro}}} \cdot E} \rightarrow \left(\frac{T_{\text{ce}}}{T_{\text{ro}}} \right)_{\text{ce}} = \frac{1}{\frac{T_{\text{ro}}}{m_{\text{ro}} \cdot f} \cdot E}$$

waarbij de thrust-to-weight ratio gelijk is na de wing loading.

$$* \frac{T_{\text{ce}}}{T_{\text{ro}}} = (0,0013 \mu - 0,0397) \frac{1}{\text{km}} \cdot h_{\text{ce}} - 0,0248 \mu + 0,7125$$

$$h_{\text{ce}} = \frac{\frac{T_{\text{ce}}}{T_{\text{ro}}} + 0,0248 \mu - 0,7125}{0,0013 \mu - 0,0397}$$

* Omdat de temperatuur i.f. kan gesteld worden van de hoogte:

$$\left. \begin{aligned} T_{\text{troposfeer}} &= 288,15 - 0,0065 \cdot h_{\text{ce}} \\ T_{\text{stratosfeer}} &= 216,5 \text{ K} \end{aligned} \right\} \text{als } T_T < T_S \Rightarrow T_S \text{ geldt.}$$

* Snelheid a is ook een functie van de temperatuur

$$a = 20,5 \cdot \sqrt{T_x}$$

* $V_{\text{ce}} = M \cdot a$ met M is gekend.

Reverse Engineering

* V_{cr} en Π zijn gekend $\Rightarrow a = \frac{V_{cr}}{\Pi}$
↳ data \Rightarrow wrong? \rightarrow Bepent?

$$* \quad T_x = \left(\frac{a}{20,05} \right)^2 \rightarrow \text{als } T_x < 216,65 \text{ K} \Rightarrow T_x = T_s$$

anders $T_x = T_T$

The temperature normally has a value that is included by the troposphere.

$$* \quad h_{cr} = \frac{288,15 - T_{\text{troposphere}}}{0,0065}$$

$$* \quad \frac{T_{cr}}{T_{To}} = (0,0013 \mu - 0,0397) \cdot h_{cr} - 0,0248 \mu + 0,7125$$

$$* \quad E = \left(\frac{T_{To}}{m_{To} \cdot p} \cdot \frac{T_{cr}}{T_{To}} \right)^{-1}$$

$$* \quad E_{max} = \frac{E \cdot \left(\frac{C_{lim}}{C_i} + \frac{C_i}{C_{lim}} \right)}{2}$$

Assume that $\frac{T}{W}$ and $\frac{W}{S}$ is known.

$$\textcircled{I} \quad \frac{m_{nl}}{S_w} = k_L \cdot \sqrt{\Delta_{LFL}} \cdot C_{L,max,L} \quad \text{where } \Delta_{LFL} = \left(\frac{V_{app}}{k_{app}} \right)^2$$

$$\text{and} \quad \frac{m_{nro}}{S_w} = \frac{m_{nl}}{S_w} \cdot \frac{m_{nro}}{m_{nl}}$$

$$\Rightarrow \quad C_{L,max,L} = \frac{\frac{m_{nro}}{S_w} \cdot \frac{m_{nl}}{m_{nro}}}{k_L \cdot \sqrt{\Delta_{LFL}}}$$

$$\textcircled{To} \quad \frac{T_{ro}}{m_{nro} \cdot g} = \alpha \cdot \frac{m_{nro}}{S_w} = \frac{k_{ro}}{\Delta_{TOFL} \cdot \sqrt{\Delta_{L,max,ro}}} \cdot \frac{m_{nro}}{S_w}$$

$$\Rightarrow \quad C_{L,max,ro} = \frac{k_{ro}}{\Delta_{TOFL} \cdot \sqrt{\Delta_{L,max,ro}}} \cdot \frac{m_{nro}/S_w}{T_{ro}/m_{nro} \cdot g}$$

$$\textcircled{gnd} \quad \frac{T_{ro}}{m_{nro} \cdot g} = \frac{n_E}{n_E - 1} \cdot \left(\frac{1}{E_{ro}} + \sin \gamma \right)$$

$$\Rightarrow \quad E_{ro} = \left(\frac{T_{ro}}{m_{nro} \cdot g} \cdot \frac{n_E - 1}{n_E} - \sin \gamma \right)^{-1} = \frac{C_{L,ro}}{C_{D,p} + \frac{C_{L,ro}^2}{\pi \cdot e \cdot A}}$$

→ zijn ze gelijk in excel?

$$\textcircled{IIA} \quad \frac{T_{ro}}{m_{nl} \cdot g} = \frac{n_E}{n_E - 1} \cdot \left(\frac{1}{E_L} + \sin \gamma \right)$$

$$\frac{T_{ro}}{m_{nro} \cdot g} = \frac{n_E}{n_E - 1} \cdot \left(\frac{1}{E_L} + \sin \gamma \right) \cdot \frac{m_{nl}}{m_{nro}}$$

$$\Rightarrow \quad E_L = \left(\frac{T_{ro}}{m_{nro} \cdot g} \cdot \frac{n_E - 1}{n_E} \cdot \frac{m_{nro}}{m_{nl}} - \sin \gamma \right)^{-1} = \frac{C_{L,L}}{C_{D,p} + \frac{C_{L,L}^2}{\pi \cdot e \cdot A}}$$

→ komt dit overeen in excel.

© Formulas which involve E_{max} :

$$C_{D0} = \frac{\bar{v} \cdot A \cdot e}{4 \cdot E_{max}^2} \longrightarrow C_{D,nd} = \sqrt{C_{D0} \cdot A \cdot e \cdot \bar{v}}$$

$$\longrightarrow C_L = \frac{C_{D,nd}}{(V/V_{nd})^2}$$

$$E = \frac{2 \cdot E_{max}}{\frac{1}{C_L/C_{L,nd}} + \frac{C_L}{C_{L,nd}}}$$

Relation with wing loading and thrust to weight ratio:

$$\frac{M_{TTO}}{S_w} = \frac{C_L \cdot \pi^2}{g} \cdot \frac{\gamma}{2} \cdot \rho_0 \cdot (1 - 0,02256 \cdot h)^{5,258}$$

$$\frac{T_{T0}}{m_{TTO} \cdot g} = \frac{1}{(T_{CL}/T_{T0}) \cdot E} \longrightarrow \frac{T_{CL}}{T_{T0}} = (0,0013\mu - 0,0397) \cdot h - 0,0248\mu + 0,7125$$

Altitude as a function, expressed in 'km':

$$h = \frac{1}{0,02256} \cdot \left[1 - \left(\frac{2 \cdot g \cdot M_{TTO}/S_w}{C_L \cdot \pi^2 \cdot \gamma \cdot \rho_0} \right)^{\frac{1}{5,258}} \right]$$

$$h = \frac{\frac{T_{CL}}{T_{T0}} + 0,0248\mu - 0,7125}{0,0013\mu - 0,0397}$$

Composing equation for E_{max} :

$$E = \frac{2 \cdot E_{max}}{\frac{1}{C_L/C_{L,nd}} + \frac{C_L}{C_{L,nd}}} = \frac{1}{\frac{T_{CL}}{T_{T0}} \cdot \frac{T_{T0}}{m_{TTO} \cdot g}}$$

$$E_{max} \cdot \frac{2 \cdot \frac{T_{CL}}{T_{T0}} \cdot \frac{T_{T0}}{m_{TTO} \cdot g}}{\frac{1}{C_L/C_{L,nd}} + \frac{C_L}{C_{L,nd}}} - 1 = 0$$

$$\text{with } \frac{2 \cdot \frac{T_{ro}}{m_{pro} \cdot g}}{\frac{1}{C/C_{nd}} + \frac{C}{C_{nd}}} = z$$

$$E_{max} \cdot z \cdot \frac{T_{cr}}{T_{ro}} - 1 = 0$$

$$z \cdot E_{max} \cdot ((0,0013 \mu - 0,0397)h - 0,0248 \mu + 0,7125) - 1 = 0$$

$$z \cdot E_{max} \cdot \left[\frac{0,0013 \mu - 0,0397}{0,02256} \cdot \left(1 - \left(\frac{2 \cdot g \cdot m_{pro} / S_w}{C \cdot \pi^2 \cdot r \cdot p_0} \right)^{\frac{1}{5,258}} \right) - 0,0248 \mu + 0,7125 \right] - 1 = 0$$

$$z \cdot E_{max} \cdot \left[0,0328 \mu - 1,05 - \left(\frac{2 \cdot E_{max}}{\frac{C}{C_{nd}} \cdot \pi \cdot A \cdot e} \right)^{\frac{1}{5,258}} \cdot \left(\frac{2 \cdot g \cdot m_{pro} / S_w}{\pi^2 \cdot r \cdot p_0} \right)^{\frac{1}{5,258}} \cdot (0,0576 \mu - 1,76) \right] - 1 = 0$$

$$E_{max}^{\frac{6,258}{5,258}} \cdot \frac{2 \cdot \frac{T_{ro}}{m_{pro} \cdot g}}{\frac{1}{C/C_{nd}} + \frac{C}{C_{nd}}} \cdot \left[\frac{4 \cdot g \cdot \frac{m_{pro}}{S_w}}{\frac{C}{C_{nd}} \cdot \pi \cdot A \cdot e \cdot \pi^2 \cdot r \cdot p_0} \right]^{\frac{1}{5,258}} \cdot (0,0576 \mu - 1,76) - E_{max} \cdot \frac{2 \cdot \frac{T_{ro}}{m_{pro} \cdot g}}{\frac{1}{C/C_{nd}} + \frac{C}{C_{nd}}} \cdot (0,0328 \mu - 1,05) + 1 = 0$$

$$\frac{6,258}{5,258} \cdot E_{max}^{\frac{1}{5,258}} \cdot \frac{2 \cdot \frac{T_{ro}}{m_{pro} \cdot g}}{\frac{1}{C/C_{nd}} + \frac{C}{C_{nd}}} \cdot \left[\frac{4 \cdot g \cdot \frac{m_{pro}}{S_w}}{\frac{C}{C_{nd}} \cdot \pi \cdot A \cdot e \cdot \pi^2 \cdot r \cdot p_0} \right]^{\frac{1}{5,258}} \cdot (0,0576 \mu - 1,76) - \frac{2 \cdot \frac{T_{ro}}{m_{pro} \cdot g}}{\frac{1}{C/C_{nd}} + \frac{C}{C_{nd}}} \cdot (0,0328 \mu - 1,05) = 0$$